



- Can be solved <u>exactly</u>, but for various reasons FEA prefers to evaluate integrals like this <u>approximately</u>:
 - > <u>Historically</u>, considered more efficient and reduced coding errors.
 - > <u>Only possible approach</u> for isoparametric elements.
 - Can actually <u>improve</u> performance in certain cases!

Definite integrals can be computed numerically

$$\int_{a}^{b} f(x) dx \cong \sum_{i} w_{i} f(x_{i})$$

Dbjective:

- > Determine points x_i
- > Determine coefficients W_i





> Depending on choice of w_i and x_i

- > Midpoint Rule
- > Trapezoidal Rule
- Simpson's
- Gaussian Quadratures
- ▶ etc



Numerical Integration





Numerical Integration

It can be shown that $L(f;x_i) \leq \int_{a}^{b} f(x) dx \cong \sum_{i} w_i f(x_i) \leq U(f;x_i)$ $\lim_{i \to \infty} L(f;x_i) = \int_{a}^{b} f(x) dx = \sum_{i} w_i f(x_i) = \lim_{i \to \infty} U(f;x_i)$ Objective $\int_{a}^{b} f(x) dx \cong \sum_{i} w_i f(x_i) = w_1 f(x_1) + w_2 f(x_2) + \dots + w_n f(x_n)$

Where do such formulae come from?

Theory of Interpolation....

Let
$$f(x) \approx p(x) = \sum_{i=1}^{n} l_i(x) f(x_i)$$
 $l_i(x)$: cardinal functions
Recall Shape Functions



Numerical Integration: Quadratures

$$\int_{a}^{b} f(x) dx \approx \int_{a}^{b} p(x) dx = \sum_{i=1}^{n} f(x_{i}) \int_{a}^{b} l_{i}(x) dx = \sum_{i=1}^{n} f(x_{i}) w_{i}$$

It will give correct values for the integral of every polynomial of degree $\leq n-1$

Gaussian Quadrature:

Karl Friedriech Gauss discovered that by a special placement

of nodes the accuracy of the numerical integration could be

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greatly increased
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1.

Numerical Integration: Gaussian Quadrature

Theorem on Gaussian nodes

Let q be a polynomial of degree n such that

$$\int_{a}^{b} q(x) x^{k} dx = 0 \qquad k = 0, 1, ..., n - 1$$

Let x_1, x_2, \dots, x_n be the roots of q(x). Then

$$\int_{a}^{b} f(x) dx \cong \sum_{i} w_{i} f(x_{i}) = w_{1} f(x_{1}) + w_{2} f(x_{2}) + \dots + w_{n} f(x_{n})$$

with x_i 's as nodes is exact for all polynomials of degree $\leq 2n-1$.



Assume two point formulation, then:

$$F(\xi)d\xi = w_1F(\xi_1) + w_2F(\xi_2)$$

Four equations are created using Legendre polynomials $(1, \xi, \xi^2, \xi^3)$

$$w_{1}F(\xi_{1}) + w_{2}F(\xi_{2}) = \int_{-1}^{1} 1d\xi = 2$$

$$w_{1}F(\xi_{1}) + w_{2}F(\xi_{2}) = \int_{-1}^{1} \xi d\xi = 0$$

$$w_{1}(I) + w_{2}(I) = 2$$

$$w_{1}(\xi_{1}) + w_{2}(\xi_{2}) = 0$$

$$w_{1}(\xi_{1}) + w_{2}(\xi_{2}) = 0$$

$$w_{1}(\xi_{1})^{2} + w_{2}(\xi_{2})^{2} = 2/3$$

$$w_{1}(\xi_{1})^{2} + w_{2}(\xi_{2})^{2} = 2/3$$

$$\xi_{1} = -1/\sqrt{3}$$

$$w_{1}F(\xi_{1}) + w_{2}F(\xi_{2}) = \int_{-1}^{1} \xi^{3}d\xi = 0$$





One Dimensional Gauss Integration Rules:

 $\xi = -1$



Weighting Factors & Sampling Points for Gauss-Legendre Formula

Points(n)	Weighting Factor (w_i)	Sampling Points (ξ_i)
2	$w_1 = 1.00000000$ $w_2 = 1.00000000$	$\xi_1 =577350269$ $\xi_2 = 577350269$
	$w_2 = 0.55555556$	$\xi_2 =774596669$
3	$w_2 = 0.88888889$ $w_2 = 0.5555556$	$\xi_2 = 0.0$ $\xi_2 = 0.774596669$
	$w_3 = 0.3355555555555555555555555555555555555$	$\xi_3 = 0.774330003$ $\xi_1 =861136312$
4	$w_2 = 0.6521452$	$\xi_2 =339981044$
	$w_3 = 0.0321432$ $w_1 = 0.3478548$	$\xi_3 = 0.339981044$ $\xi_4 = .861136312$
	$w_1 = 0.2369269$	$\xi_1 =906179846$
	$w_2 = 0.4786287$	$\xi_2 =538469310$
5	$w_3 = 0.5688889$	$\xi_3 = 0.0$
	$w_4 = 0.4786287$	$\xi_4 = .538469310$
	$w_5 = 0.2369269$	$\xi_5 = .906179846$



Example:

$$I = \int_{2}^{6} (x^{2} + 5x + 3)dx = ?$$
Analytical solution $\rightarrow 161.3333$

$$x = 4 + 2\xi \rightarrow I = \int_{-1}^{1} 2[(4 + 2\xi)^{2} + 5(4 + 2\xi) + 3]d\xi$$

$$F(\xi)$$

$$I = w_{1}F(\xi_{1}) + w_{2}F(\xi_{2}) = F(\frac{1}{\sqrt{3}}) + F(\frac{-1}{\sqrt{3}})$$

I = (1)(50.64445) + (1)(110.68888) = 161.3333

Two Dimensional Product Gauss Rules

Canonical form of integral:

$$\int_{-1}^{1} \int_{-1}^{1} F(\xi, \eta) \, d\xi \, d\eta = \int_{-1}^{1} d\eta \int_{-1}^{1} F(\xi, \eta) \, d\xi$$

Gauss integration rules with p_1 points in the ξ direction and p_2 points in the η direction:

$$\int_{-1}^{1} \int_{-1}^{1} F(\xi, \eta) \, d\xi \, d\eta = \int_{-1}^{1} d\eta \int_{-1}^{1} F(\xi, \eta) \, d\xi \approx \sum_{i=1}^{p_1} \sum_{j=1}^{p_2} w_i w_j F(\xi_i, \eta_j)$$

Usually p1 = p2 = p



2-Dimensional Integration: Gaussian Quadrature

$$\int_{-1-1}^{1} \int_{-1-1}^{1} f(\xi,\eta) d\xi d\eta \cong \int_{-1}^{1} \left[\sum_{i=1}^{n} w_i f(\xi_i,\eta) \right] d\eta \approx \sum_{j=1}^{n} \sum_{i=1}^{n} w_j w_i f(\xi_i,\eta_j)$$





Graphical Representation of the First Four 2D

Product-Type Gauss Integration Rules



With Equal # of Points *p* in Each Direction









Modeling Issues: Element Shape

Square : Optimum Shape Not always possible to use



Rectangles: Rule of Thumb Ratio of sides <2

Larger ratios may be used with caution



Angular Distortion Internal Angle < 180°

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Modeling Issues: Degenerate Quadrilaterals Coincident Corner Nodes





Less accurate



Modeling Issues: Degenerate Quadrilaterals Three nodes collinear





<u>2</u>

Less accurate



Do not use in place of triangular elements





Modeling Issues: Degenerate Quadrilaterals





Convergence Considerations

For monotonic convergence of solution; Requirements

Elements (mesh) must be compatible

Elements must be complete



Mesh compatibility - Refinement



Acceptable Transition

Compatibility of displacements OK Stresses?

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Gauss integration

• For evaluation of integrals in **k** (in practice)

In 1 direction:
$$I = \int_{-1}^{+1} f(\xi) d\xi = \sum_{j=1}^{m} w_j f(\xi_j)$$

m gauss points gives exact solution of polynomial integrand of n = 2m - 1

In 2 directions:
$$I = \int_{-1}^{+1} \int_{-1}^{+1} f(\xi, \eta) d\xi d\eta = \sum_{i=1}^{n_x} \sum_{j=1}^{n_y} w_i w_j f(\xi_i, \eta_j)$$



Example:



<u>Given</u>: 4-node plane stress element has E = 30,000 ksi, v = 0.25, h = 0.50 in, no body force, and surface traction shown.
 Dequired: Find k and f Use 2 x 2 Cause quadrature for k

 \blacktriangleright <u>Required</u>: Find **k** and **f**. Use 2 x 2 Gauss quadrature for **k**.



Solution:

> Isoparametric mapping:

$$\begin{aligned} x &= \frac{1}{4} \left(1 - \xi \right) \left(1 - \eta \right) x_1 + \frac{1}{4} \left(1 + \xi \right) \left(1 - \eta \right) x_2 + \frac{1}{4} \left(1 + \xi \right) \left(1 + \eta \right) x_3 + \frac{1}{4} \left(1 - \xi \right) \left(1 + \eta \right) x_4 \\ &= \frac{1}{4} \left(1 - \xi \right) \left(1 - \eta \right) * 4 + \frac{1}{4} \left(1 + \xi \right) \left(1 - \eta \right) * 8 + \frac{1}{4} \left(1 + \xi \right) \left(1 + \eta \right) * 11 + \frac{1}{4} \left(1 - \xi \right) \left(1 + \eta \right) * 2 \\ &= \frac{25}{4} + \frac{13}{4} \xi + \frac{1}{4} \eta + \frac{5}{4} \xi \eta; \\ y &= \frac{1}{4} \left(1 - \xi \right) \left(1 - \eta \right) * 3 + \frac{1}{4} \left(1 + \xi \right) \left(1 - \eta \right) * 4 + \frac{1}{4} \left(1 + \xi \right) \left(1 + \eta \right) * 10 + \frac{1}{4} \left(1 - \xi \right) \left(1 + \eta \right) * 8 \\ &= \frac{25}{4} + \frac{3}{4} \xi + \frac{11}{4} \eta + \frac{1}{4} \xi \eta; \end{aligned}$$

> Jacobian matrix and Jacobian:

$$\mathbf{J} = \begin{bmatrix} \frac{\partial x}{\partial \xi} & \frac{\partial y}{\partial \xi} \\ \frac{\partial x}{\partial \eta} & \frac{\partial y}{\partial \eta} \end{bmatrix} = \begin{bmatrix} \frac{13}{4} + \frac{5}{4}\eta & \frac{3}{4} + \frac{1}{4}\eta \\ \frac{1}{4} + \frac{5}{4}\xi & \frac{11}{4} + \frac{1}{4}\xi \end{bmatrix}; \quad J = \det \mathbf{J} = \frac{35}{4} - \frac{1}{8}\xi + \frac{27}{8}\eta.$$



B matrix:

$$\begin{bmatrix} B(\xi,\eta) \end{bmatrix} = \frac{l}{|\mathbf{J}|} \begin{bmatrix} B_1 \mid B_2 \mid B_3 \mid B_4 \end{bmatrix}$$

$$\begin{bmatrix} B_i \end{bmatrix} = \begin{bmatrix} a(N_{i,\xi}) - b(N_{i,\eta}) & 0 \\ 0 & c(N_{i,\eta}) - d(N_{i,\xi}) \\ c(N_{i,\eta}) - d(N_{i,\xi}) & a(N_{i,\xi}) - b(N_{i,\eta}) \end{bmatrix}$$



B matrix:

$$\begin{split} N_{1,\xi} &= \frac{\partial N_1}{\partial \xi} = \frac{-1(1-\eta)}{4} = \frac{(\eta-1)}{4} \\ N_{1,\eta} &= \frac{\partial N_1}{\partial \eta} = \frac{(1-\xi)(-1)}{4} = \frac{(\xi-1)}{4} \\ N_{2,\xi} &= \frac{\partial N_2}{\partial \xi} = \frac{(1)(1-\eta)}{4} = \frac{(1-\eta)}{4} \\ N_{2,\eta} &= \frac{\partial N_2}{\partial \eta} = \frac{(1+\xi)(-1)}{4} = \frac{-(\xi+1)}{4} \\ N_{3,\xi} &= \frac{\partial N_3}{\partial \xi} = \frac{(1)(1+\eta)}{4} = \frac{(1+\eta)}{4} \\ N_{3,\eta} &= \frac{\partial N_3}{\partial \eta} = \frac{(1+\xi)(1)}{4} = \frac{(\xi+1)}{4} \\ N_{4,\xi} &= \frac{\partial N_4}{\partial \xi} = \frac{(-1)(1+\eta)}{4} = \frac{-(1+\eta)}{4} \\ N_{4,\eta} &= \frac{\partial N_4}{\partial \eta} = \frac{(1-\xi)(1)}{4} = \frac{(1-\xi)}{4} \end{split}$$

$$a = 1/4 \left[y_1(\xi - 1) + y_2(-\xi - 1) + y_3(\xi + 1) + y_4(1 - \xi) \right]$$

$$b = 1/4 \left[y_1(\eta - 1) + y_2(1 - \eta) + y_3(\eta + 1) + y_4(-1 - \eta) \right]$$

$$c = 1/4 \left[x_1(\eta - 1) + x_2(1 - \eta) + x_3(\eta + 1) + x_4(-1 - \eta) \right]$$

$$d = 1/4 \left[x_1(\xi - 1) + x_2(-\xi - 1) + x_3(\xi + 1) + x_4(1 - \xi) \right]$$



B matrix:

$$\mathbf{B} = \frac{1}{70 - \xi + 27\eta} \times$$

 $\begin{bmatrix} -4+6\eta-2\xi & 0 & 7-5\eta+2\xi & 0 & 4+5\eta-\xi & 0 & -7-6\eta+\xi & 0 \\ 0 & -6-3\eta+9\xi & 0 & -7-2\eta-9\xi & 0 & 6+2\eta+4\xi & 0 & 7+3\eta-4\xi \\ -6-3\eta+9\xi & -4+6\eta-2\xi & -7-2\eta-9\xi & 7-5\eta+2\xi & 6+2\eta+4\xi & 4+5\eta-\xi & 7+3\eta-4\xi & -7-6\eta+\xi \end{bmatrix}$



▶ k matrix:



<u>Problem 1</u>

Figure (1) shows a four-node quadrilateral. The (x,y) coordinates of each node are given in the figure. The element displacement vector u is given as: U=[0,0,0.20,0,0.15,0.10,0,0.05]Find:

A- The x-y coordinates of a point *P* whose location in the master element is given by $\xi = 0.5, \eta = 0.5$

B- The u and v displacement of the point P

<u>Problem 2</u>

Using a 2 by 2 rule evaluate the following integral by Gaussian quadrature, where a denotes the region shown in Figure (1).

$$\iint_A (x^2 + xy^2) dx dy$$



Figure (1)



Zero-Energy Modes (Mechanisms; Kinematic Modes) –

- Instabilities for an element (or group of elements) that produce deformation without any strain energy.
- Typically caused by using an inappropriately low order of Gauss quadrature.
- If present, will dominate the deformation pattern.

Can occur for all 2D elements <u>except</u> the CST.



Zero-Energy Modes –

Deformation modes for a bilinear quad:



#1, #2, #3 = *rigid body modes*; can be eliminated by proper constraints.
#4, #5, #6 = *constant strain modes*; <u>always</u> have nonzero strain energy.
#7, #8 = *bending modes*; produce <u>zero</u> strain at origin.



Zero-Energy Modes -

Mesh instability for bilinear quads using order 1 quadrature:



"Hourglass modes"



Zero-Energy Modes -

Element instability for quadratic quadrilaterals using 2x2 Gauss quadrature:



"Hourglass modes"



Zero-Energy Modes -

- How can you prevent this?
 - Use higher order Gauss quadrature in formulation.
 - Can artificially "stiffen" zero-energy modes via penalty functions.
 - Avoid elements with known instabilities!



The gauss points for a triangular region differ from the square region considered earlier. The simplest one is the one-point rule at the centroid with weight $w_1 = 1/2$ and $\xi_1 = \eta_1 = \zeta_1 = 1/3$



Gauss Integration for Triangular Region

First set of quadrature rules for triangular elements









Second set of quadrature rules for triangular elements













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Gauss Integration for Triangular Region

$$\int_{0}^{1} \int_{0}^{1-\xi} f(\xi,\eta) d\eta d\xi \approx \sum_{i=1}^{n} w_i f(\xi_i,\eta_i)$$

No. of Points (n)	Weight ${\cal W}_i$	Multiplicity	ξ_i	η_i	${\boldsymbol{\zeta}}_i$
One	1/2	1	1/3	1/3	1/3
Three	1/6	3	2/3	1/6	1/6
Three	1/6	3	1/2	1/2	0
Four	-9/32 25/96	1 3	1/3 3/5	1/3 1/5	1/3 1/5
Six	1/12	6	0.6590276223	0.231933685	0.109039009

Because of triangular symmetry, the Gauss point are occurred in group or *multiplicity* of one, three or six. For multiplicity of three if one Gauss point is at (2/3, 1/6, 1/6) then the other two Gauss points are located at (1/6, 2/3, 1/6) and (1/6, 1/6, 2/3). For multiplicity of six all six possible permutation of three coordinate are used.

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Appendix Weights Triangular Order No. Figure Rem. Points Coordinates W_k $R = O(h^2)$ a $\frac{1}{3}, \frac{1}{3}, \frac{1}{3}$ 1 Linear 1 $\begin{array}{cccc} a & \frac{1}{2}, \frac{1}{2}, 0 & \frac{1}{3} \\ R = 0(h^3) & b & 0, \frac{1}{2}, \frac{1}{2} & \frac{1}{3} \\ c & \frac{1}{2}, 0, \frac{1}{2} & \frac{1}{3} \end{array}$ Quadratic 2 $\frac{1}{3}, \frac{1}{3}, \frac{1}{3}$ -27/48а b 0.6, 0.2, 0.2 25/48 $R=0(h^4)$ 3 Cubic 0.2, 0.6, 0.2 25/48 с 0.2, 0.2, 0.6 d 25/48 $\frac{1}{3}, \frac{1}{3}, \frac{1}{3}$ 0.225 а b $\alpha_1, \beta_1, \beta_1$ $\beta_1, \alpha_1, \beta_1$ 0.13239415 с $R=0(h^6)$ d Quintic $\beta_1, \beta_2, \beta_2$ 5 $\alpha_2, \beta_2, \beta_2$ е f 0.12593918 $\beta_2, \alpha_2, \beta_2$ $\beta_2, \beta_2, \alpha_2$ g With: $\alpha_1 = 0.05961587$ $\beta_1 = 0.47014206$ $\alpha_2 = 0.79742699$ $\beta_2 = 0.10128651$

TABLE 5.3. Numerical Integration Formulas for Triangles

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